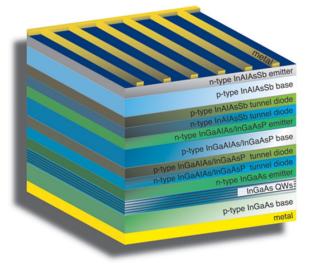
# Lecture 10 - 20/11/2024

## The *p-n* junction

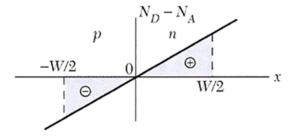
- I-V characteristic: non ideal case
- Breakdown voltage
- Zener diode
- Avalanche diode
- Tunneling diode
- Solar cells



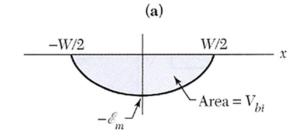
# **Summary Lecture 10**

#### Linearly graded *p-n*-junction:

$$\frac{d^2\phi}{dx^2} = -\frac{\rho}{\varepsilon} = -\frac{q\alpha}{\varepsilon}x$$



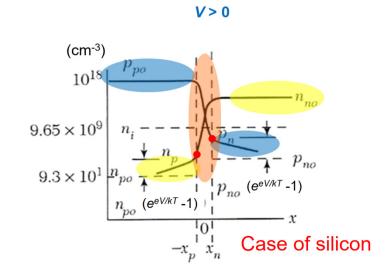
Impurity distribution



Electric field distribution

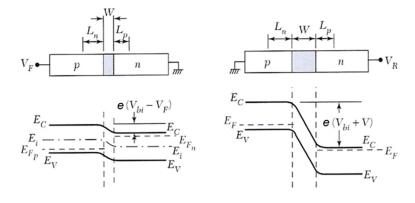
$$V_{bi} = \frac{2k_{B}T}{3e} \ln \left( \frac{\alpha^{2} \varepsilon k_{B}T}{8e^{2} n_{i}^{3}} \right)$$

All known parameters!



# **Summary Lecture 10**

Out of equilibrium/under bias: LLI



Quasi Fermi level:

$$E_{F_n} = E_C - k_B T \ln\left(\frac{N_C}{n}\right) \text{ with } n = n_0 + G_n \tau_n$$

$$E_{F_p} = E_V + k_B T \ln\left(\frac{N_V}{p}\right) \text{ with } p = p_0 + G_p \tau_p$$

$$\Delta p$$

$$J = J_{n}(-x_{p}) + J_{p}(x_{n})$$

$$= \frac{eD_{n}n_{p0}}{L_{n}}(e^{eV/k_{B}T} - 1) + \frac{eD_{p}p_{n0}}{L_{p}}(e^{eV/k_{B}T} - 1)$$

$$J(V) = J_{S} \left( \exp \left( \frac{eV}{k_{B}T} \right) - 1 \right)$$

The assumption we made regarding the absence of currents in the space charge region is quite rough.

Actually, there is often a non-negligible contribution to the current due to recombination and generation processes occurring in the depletion region (in Si and GaAs p-n junctions because  $n_i$  is small, electron and hole emissions occur through bandgap generation-recombination centers located near the intrinsic Fermi level (e.g., Au and Cu in silicon and Cr in GaAs junctions))

For contacting

To get resistive layers

#### The total current density then writes

$$J = J_p + J_n + J_{r,g}$$

$$J \approx J_{p,diff} + J_{n,diff} + J_{r,g}$$

Under forward bias, the diffusion current dominates over the drift one!

#### Generation and recombination currents in the space charge region

$$r > 0$$
 recombination rate  $r < 0$  generation rate  $r$ 

e-book by Sze

1) Reverse bias: generation current

-V >> 
$$k_{\rm B}T/e \Rightarrow r \approx -\frac{n_{\rm i}}{2\tau_{\rm e}}$$
 then

Because  $n$  and  $p << n_{\rm i}$  in the reverse bias

Fiftective of

Because 
$$n$$
 and  $p \ll n_i$  in the reverse bias regime

$$J_{\rm g} = -\frac{e n_{\rm i}}{2\tau_{\rm e}} W$$

Effective generation lifetime

$$W = \sqrt{\frac{2\varepsilon}{e} \left(\frac{N_{A} + N_{D}}{N_{A}N_{D}}\right) (V_{bi} - V)}$$

$$eV_{bi} = E_{g} - k_{B}T \ln \left( \frac{N_{v}N_{c}}{N_{A}N_{D}} \right)$$

2) Forward bias: recombination current Cf. Shockley's relations

r maximum for 
$$n + p$$
 minimum (i.e.,  $n = p$ ) and  $np = cst$   $\Rightarrow n_n = p_n = n_i exp(eV/2k_BT)$ 

$$r_{max} = \frac{1}{\tau_e} \frac{n_i^2 (e^{eV/k_BT} - 1)}{2n_i (1 + e^{eV/2k_BT})} \qquad V >> k_BT/e \Rightarrow r_{max} = \frac{n_i e^{eV/2k_BT}}{2\tau_e}$$

Effective recombination lifetime  $\propto N_t^{-1}$ 

Finally, 
$$J_{\rm r} = \frac{e n_{\rm i}}{2 \tau_{\rm e}} W_{\rm eff}$$
 with

with 
$$W_{\text{eff}} = W e^{eV/2k_BT}$$

## **Experimental** *I-V* curves

 $10^{-1}$  $T = 300 \, \text{K}$  $10^{-3}$  $\widehat{S}_{1}^{5}$  10<sup>-5</sup>  $10^{-7}$  $10^{-9}$ 0.2 1.0 1.2 0.4 0.6 0.8 0  $V_F(V)$ 

Total forward current density can be approximated, for  $p_{n0}$  >>  $n_{p0}$  (one-sided abrupt  $p^+$ -n junction) and  $V \ge 3k_BT/e$ 

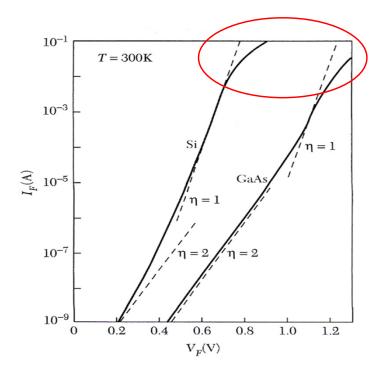
$$J_{F} = e \sqrt{\frac{D_{p}}{\tau_{p}}} \frac{n_{i}^{2}}{N_{D}} e^{eV/k_{B}T} + \frac{eWn_{i}}{2\tau_{e}} e^{eV/2k_{B}T}$$

$$\Rightarrow J_{F} \propto \exp\left(\frac{eV}{\eta k_{B}T}\right)$$

#### $\eta$ ideality factor:

- $\eta$  = 1 when ideal diffusion current dominates
- $\eta$  = 2 when recombination current dominates

$$J(V) = J_{S} \left( \exp \left( \frac{eV}{\eta k_{B}T} \right) - 1 \right)$$



#### **Series resistance and high-injection**

At high current levels,  $\eta$  > 1 and increases continuously with the forward voltage

#### 1. Series resistance

Low and medium current levels: The potential drop  $IR_s$  across neutral regions remains small vs.  $k_BT/e$  (silicon diode with  $R_s$  = 1.5 ohms,  $IR_s$  drop at 1 mA only 1.5 mV (vs.  $k_BT/e$  of 26 mV at 300 K))

High current level: 100 mA, potential drop  $IR_s$  of 0.15 V (value six times larger than  $k_BT/e$ )  $\Rightarrow$  decrease of the bias across the depletion region

$$I \approx I_{s}e^{(e(V-R_{s}I))/\eta k_{B}T} = \frac{I_{s}e^{eV/\eta k_{B}T}}{e^{eR_{s}I/\eta k_{B}T}}$$

#### 2. High-injection condition

$$p_{n}(x = x_{n}) \approx n_{n} \approx n_{i} \exp(eV/2k_{B}T) \operatorname{since}(p_{n}n_{n}) \approx p_{n_{0}}n_{n_{0}}e^{eV/k_{B}T} = n_{i}^{2} \exp(eV/k_{B}T)$$

$$\Rightarrow I \propto \exp(eV/2k_{B}T)$$
Mass action's law extended to the out of equilibrium.

Mass action's law extended to the out of equilibrium case

# Specific *p-n* junctions: Zener, avalanche and tunneling diodes, solar cells

# Reverse breakdown voltage

When the junction is reverse-biased ( $V_r$ ), both the space charge region extent and the built-in electric field vary as  $V_{eff}^{1/2}$  (where  $V_{eff} = V_{bi} + V_r$ ),

Abrupt junction case

$$W = \sqrt{\frac{2\varepsilon}{e} \left( \frac{N_{A} + N_{D}}{N_{A} N_{D}} \right) V_{eff}} \qquad E_{max} = 2V_{eff} / W \propto \sqrt{V_{eff}}$$

As a consequence,  $E_{\text{max}}$  increases but at a certain point:

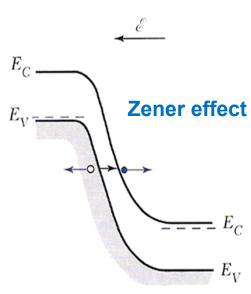
 $F = qE_{max} \Rightarrow$  material/impact ionization leading to e-h pair generation

Silicon and GaAs: E = 10<sup>6</sup> V/cm or higher (breakdown voltage)

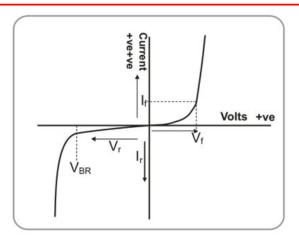
In a p-n junction this phenomenon limits the reverse bias called the **Zener voltage** ( $V_Z$ )

 $V_r > V_Z \Rightarrow$  large current: **Zener** or junction breakdown occurs

## Zener diode



 $N_{\rm A}$  and  $N_{\rm D}$  > 5 × 10<sup>17</sup> cm<sup>-3</sup> in silicon and GaAs



 $V_{\rm B} < 4E_{\rm q}/e \Rightarrow$  Zener or tunneling effect

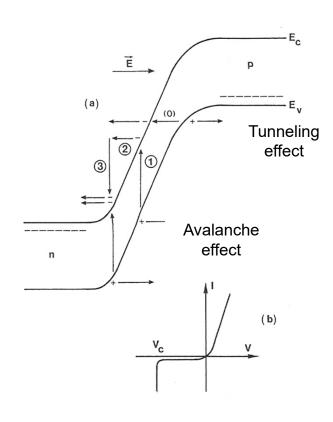
 $V_{\rm B}$  > 6 $E_{\rm g}/e$   $\Rightarrow$  avalanche multiplication

Intermediate voltages: mixture of tunneling and avalanche multiplication

A Zener diode relies on the tunneling effect: it occurs only in highly-doped p-n junctions When the doping levels are "low"  $\Rightarrow$  "avalanche" effect

Process not inherently destructive but the maximum current must be limited by an external circuit to avoid any excessive junction heating

## Avalanche diode



#### **Avalanche effect**

If the space charge region extent is large ( $W > 0.1 \mu m$ )  $\Rightarrow$  avalanche multiplication

For large reverse biases, e-h pairs are accelerated with a lot of energy, leading to breaking of lattice bonds upon collision with an atom which creates an e-h pair (*impact ionization*), newly created e-h pairs acquiring kinetic energy from the field, etc.

⇒ avalanche multiplication

Case of asymmetric p-n junctions: p<sup>+</sup>-n one-sided abrupt junction with  $N_D \le 10^{17}$  cm<sup>-3</sup>

## **Breakdown condition**

 $I_{n0}$ : incident current on the left-hand side of the depletion region of width W with W large enough so as to initiate the avalanche multiplication process

 $I_n$  increases with the distance through the depletion region to reach the value  $M_n I_{n0}$  at W  $M_n$  is the multiplication factor defined by  $M_n = I_n(W)/I_{n0}$  (similar treatment for holes)

Total current  $I = I_n + I_p$  (constant in the steady-state)

Incremental electron current at position *x* equals the number of e-h pairs generated per second in the distance *dx*:

$$d\left(\frac{I_n}{e}\right) = \left(\frac{I_n}{e}\right)(a_n dx) + \left(\frac{I_p}{e}\right)(a_p dx) \quad \text{with } a_n \text{ and } a_p \text{ the e-h ionization rates}$$

 $(a_n \text{ and } a_p \equiv \text{number of e-h pairs generated by a free carrier per unit distance traveled})$ 

$$\Rightarrow \frac{dI_n}{dx} - (a_n - a_p)I_n = a_pI$$

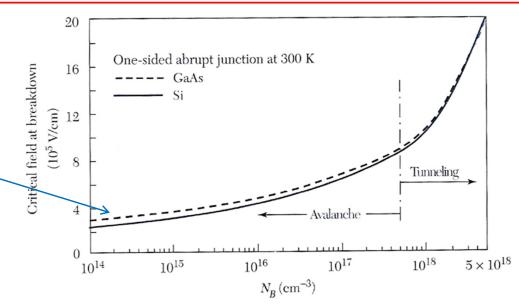
If 
$$a_n = a_p = a \Rightarrow \frac{I_n(W) - I_n(0)}{I} = \int_0^W a dx \Rightarrow 1 - \frac{1}{M_n} = \int_0^W a dx$$
 (assuming  $I_n(W) = I$ ),  $V_{B_{av}}$  obtained for  $M_n \to \infty$ , i.e.,  $\int_0^W a dx = 1$ 

Critical field at which the avalanche process occurs determined using measured  $a_n$  and  $a_p$  values + use of Poisson's equation:

$$V_{\rm B_{av}} = \frac{WE_{\rm c}}{2} = \frac{\varepsilon_{\rm r}\varepsilon_{\rm 0}E_{\rm c}^2}{2e} (N_{\rm B})^{-1}$$
  $E_{\rm c}$ : critical field  $N_{\rm B}$ : background doping lightly doped side

# Critical field and breakdown voltage

Larger  $E_c$  and hence  $V_B$  value for GaAs due to larger bandgap vs Si as the avalanche process requires band-to-band excitations



Critical field at breakdown voltage for different background doping levels ( $N_{\rm B}$ )

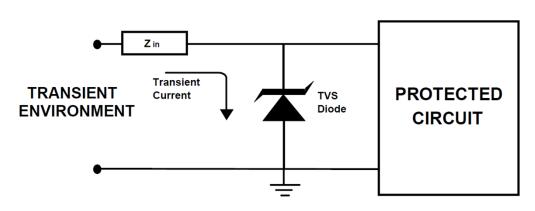
#### Approximate universal expression of $V_B$ (abrupt junction):

 $V_{\rm B} \approx 60 \left(E_{\rm g}/1.1\right)^{3/2} \left(N_{\rm B}/10^{16}\right)^{-3/4}$  V, with  $E_{\rm g}$  the room-temperature bandgap in eV and  $N_{\rm B}$  the background doping in cm<sup>-3</sup>

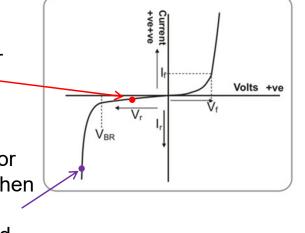
Avalanche multiplication mechanisms can generate microwave power (e.g., in IMPATT diodes) and detect optical signals as in an avalanche photodetector (high gain device used, e.g., for single photon detection)

# Zener diode: electrostatic discharge damage protection

= parallel protection element for electrical components in case of voltage spikes



- High impedance under normal operating conditions
- the transient current when the normal operating voltage of the protected circuit is exceeded

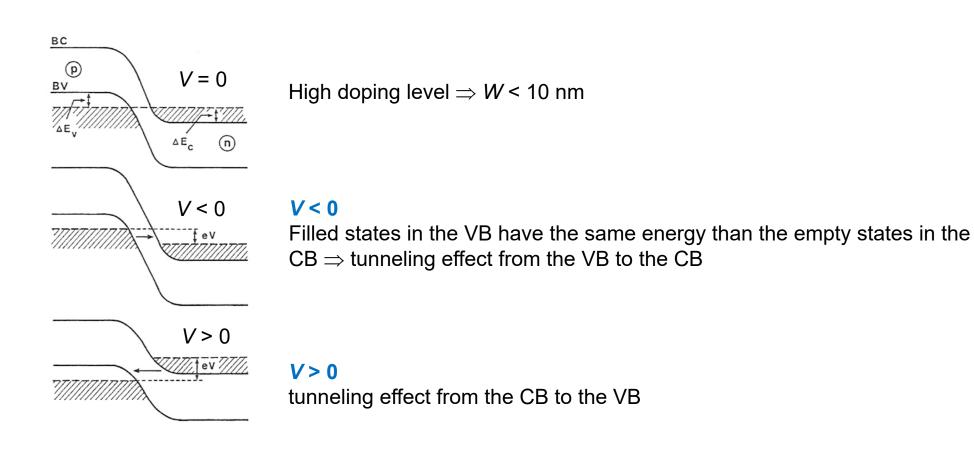


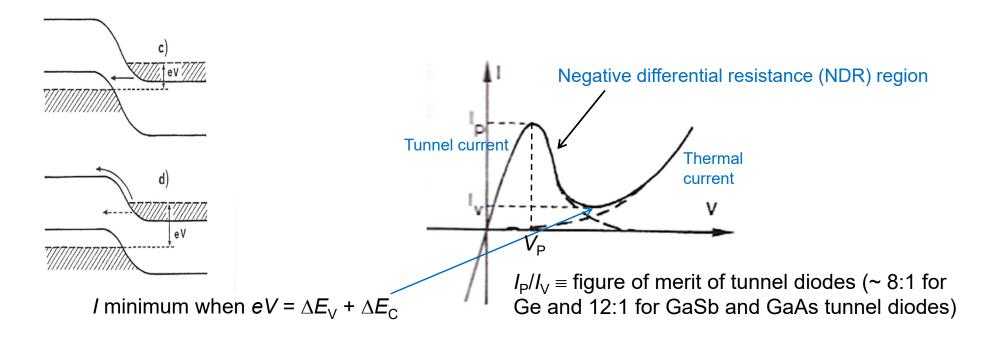


Infineon

The world smallest transient voltage suppression (TVS) diode for the protection of antennas comes from Infineon. With a footprint of just  $0.62 \times 0.32 \text{ mm}^2$  in size and 0.31 mm in height (*it cannot be too small to act as an effective heat sink*)

*n*-type and *p*-type doped layers are degenerate (quasi-Fermi levels lie in the CB and VB)





When such a diode is connected to an LC circuit (= electrical resonator) at a DC bias voltage matching the NDR region, thermal noise induced oscillations in the microwave range can be generated

The tunnel diode was invented by Leo Esaki in 1958, Nobel prize in Physics in 1973

Very short tunneling time  $\Rightarrow$  use in the mm-wave region (devices with reduced parasitic capacitance and resistance, i.e., the RC product is small)

▶ Time constant linked to cutoff frequency!

Low-power microwave applications: local oscillator, frequency-locking circuit

Transmission coefficient T of a particle through a 1D potential barrier of height  $eV_0$  and thickness d:

$$T \propto \exp(-2\beta d) = \exp\left[-2d\sqrt{2m^*(eV_0 - E)/\hbar^2}\right]$$

See, e.g., Chap. 1 of *Quantum Mechanics Vol. 1* by Cohen-Tannoudji, Diu & Laloë (Wiley-VCH, Weinheim, 2020)

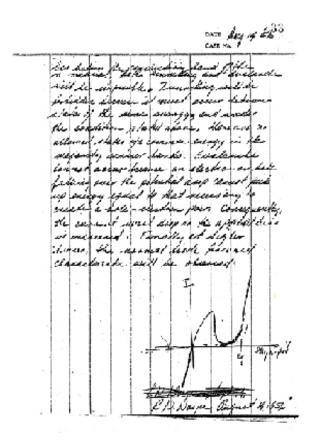
T value is finite if  $eV_0$ , d and  $m^*$  are kept small!

#### *I-V* characteristic p<sup>+</sup>-n<sup>+</sup> junction

$$I = I_{p} \left( \frac{V}{V_{p}} \right) \exp \left( 1 - \frac{V}{V_{p}} \right) + I_{0} \exp \left( \frac{eV}{k_{B}T} \right)$$
Tunnel current
Thermal current

#### **Negative differential resistance**

$$R = \left(\frac{dI}{dV}\right)^{-1} = -\left[\left(\frac{V}{V_{p}} - 1\right)\frac{I_{p}}{V_{p}}\exp\left(1 - \frac{V}{V_{p}}\right)\right]^{-1}$$





Dr. Leo Esaki joined IBM Research in 1960 and became an IBM Fellow in 1967. He was awarded the Nobel Prize in Physics in 1973 in recognition of his discovery of the tunnel diode.

# Application of diodes: solar cells

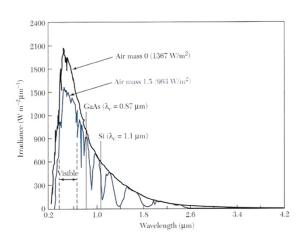
Historical article: D. M. Chaplin, C. S. Fuller, and G. L. Pearson, "A new silicon p-n junction photocell for converting solar radiation into electrical power", J. Appl. Phys. **25**, 676 (1954) (> 900 citations, 1-column long article)

Intensity of solar radiation at average distance of Earth from the sun: 1367 W/m<sup>2</sup>

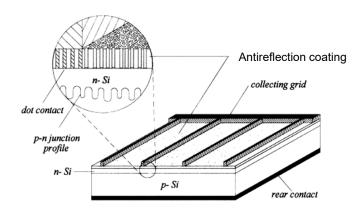
Atmosphere impact on sunlight: air mass (AM)

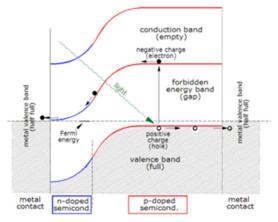
AM0: solar spectrum outside Earth's atmosphere (satellite, etc.)

AM1: sunlight at Earth's surface when the sun is overhead



Difference due to atmospheric attenuation (UV absorption in ozone, IR absorption in water vapor, scattering by airborne dust and aerosols)





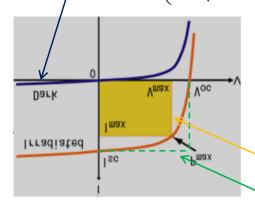
# Application of diodes: solar cells

#### Ideal <u>I-V</u> characteristic of a solar cell under illumination:

 $I \neq I_s \left(e^{eV/k_BT} - 1\right) \vdash I_L$  with  $I_L$  is the source current resulting from the excitation of excess carriers by solar radiation

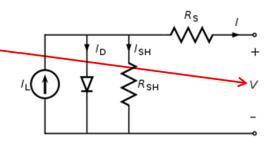
(R<sub>L</sub>, load resistance)

and 
$$J_s = A = eN_cN_v \left( \frac{1}{N_A} \sqrt{\frac{D_n}{\tau_n}} + \frac{1}{N_D} \sqrt{\frac{D_p}{\tau_p}} \right) e^{-E_g/R_B\tau}$$
 with A the device area





With a proper load, close to 80% of the product  $I_{\rm sc} V_{\rm oc}$  can be extracted (with  $I_{\rm sc} = I_{\rm L}$ )



$$V_{\text{oc}}(I=0) = \frac{k_{\text{B}}T}{e} \ln\left(\frac{I_{\text{L}}}{I_{\text{s}}} + 1\right) \approx \frac{k_{\text{B}}T}{e} \ln\left(\frac{I_{\text{L}}}{I_{\text{s}}}\right)$$

$$P = IV = I_{s}V(e^{eV/k_{B}T} - 1) - I_{L}V$$

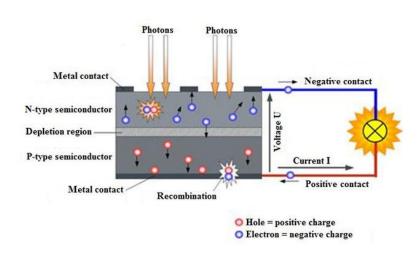
Maximum power when dP/dV = 0,

$$P_{\text{max}} = I_{\text{max}} V_{\text{max}} \approx I_{\text{L}} \left[ V_{\text{oc}} - \frac{k_{\text{B}}T}{e} \ln \left( 1 + \frac{eV_{\text{max}}}{k_{\text{B}}T} \right) - \frac{k_{\text{B}}T}{e} \right]$$

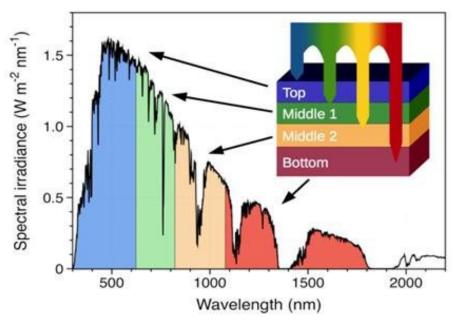
Conversion efficiency (case of a perfect solar cell, no series resistance  $R_s$ , etc.)

$$\eta = \frac{I_{\text{max}}V_{\text{max}}}{P_{\text{in}}} = \frac{FF \cdot I_{\text{L}}V_{\text{oc}}}{P_{\text{in}}} \quad \text{where } P_{\text{in}} \text{ is the incident power and } FF \text{ the fill factor defined as } FF \equiv \frac{(I_{\text{max}}V_{\text{max}})}{(I_{\text{L}}V_{\text{oc}})}$$

# Application of diodes: multi-spectral solar cells

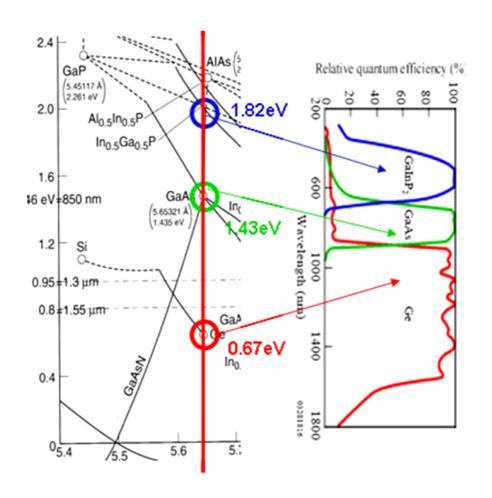


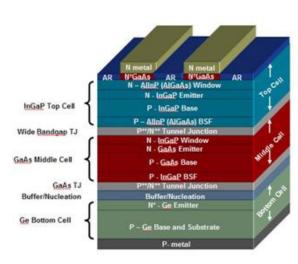
Different solar cells in series to cover the whole solar spectrum



Higher solar cell efficiency

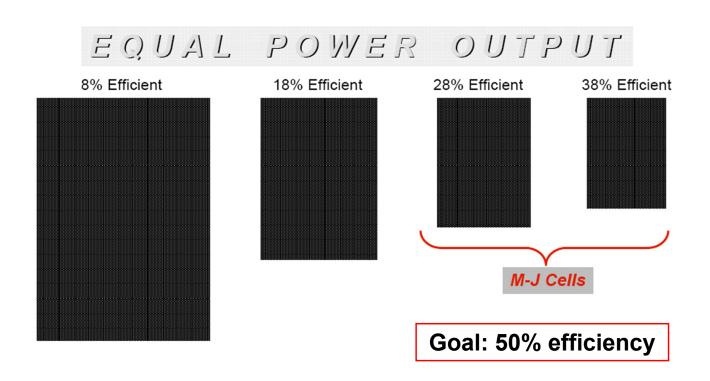
# Multi-spectral solar cells





# Multi-spectral solar cells

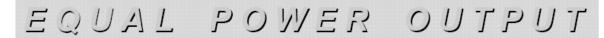
Solar Cell Efficiency makes a <u>big</u> <u>difference</u> in the size and cost of the photovoltaic element

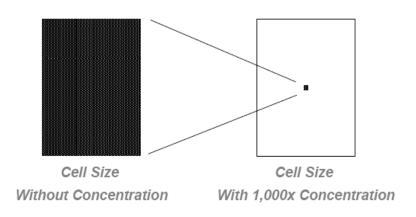


2022: 39.5% - NREL

## Solar cells with concentrator

### Concentration enables the use of very small solar cells





2023: 47.6% - NREL

## Solar cells

#### Improved cell efficiency

• More power from the same area

#### Optimized optics

Reduce lost sunlight

#### Low cost components

 Structural members can be manufactured in low cost countries

#### Heliostat

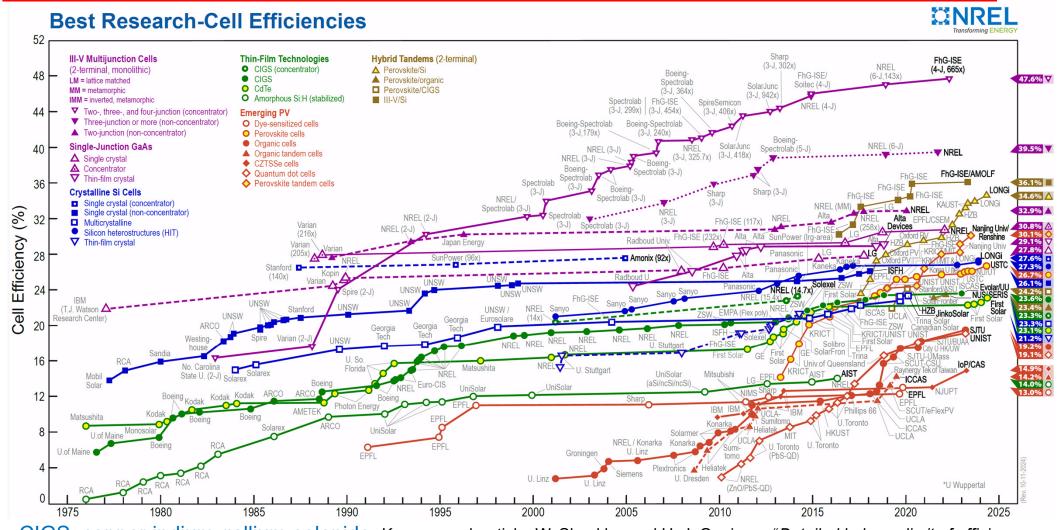
 All of the above with fewer, simpler moving parts





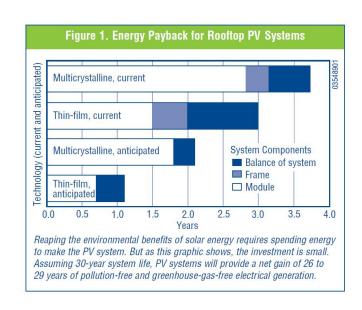
- Current cost (2020) in the USA: \$0.05-0.13/kWh
   \$0.05/kWh, a 6 kW residential system will resume to \$1.4 per Watt
- Current cost (2019) in the EU: €0.052/kWh
- ⇒ Mostly due to decrease in the cost of PV modules

# Solar cell efficiency



CIGS: copper indium gallium selenide Key research article: W. Shockley and H. J. Queisser, "Detailed balance limit of efficiency of p-n junction solar cells", J. Appl. Phys. **32**, 510 (1961) (> 10200 citations)

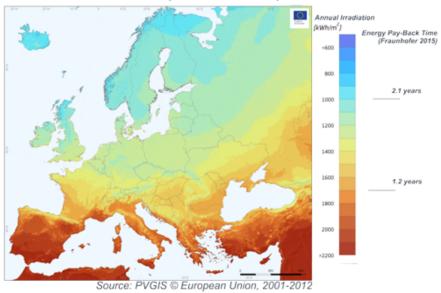
# Solar cells: payback for PV systems



#### Source: DOE/NREL

#### Multicrystalline silicon PV rooftop modules

Photovoltaic Solar Electricity Potential in European Countries



Source: Fraunhofer ISE